

Kermit's What-Happens-Next-Machine Reloaded

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Abstract. If Kermit's What-Happens-Next-Machine had functioned, you would not have seen much, because it would have gone too quickly. In this article it is shown that putting up and solving the equations of motion of a seemingly simple mechanical apparatus presents a challenging problem. The simulation can, however, be quite instructive and also entertaining.

1. Introduction

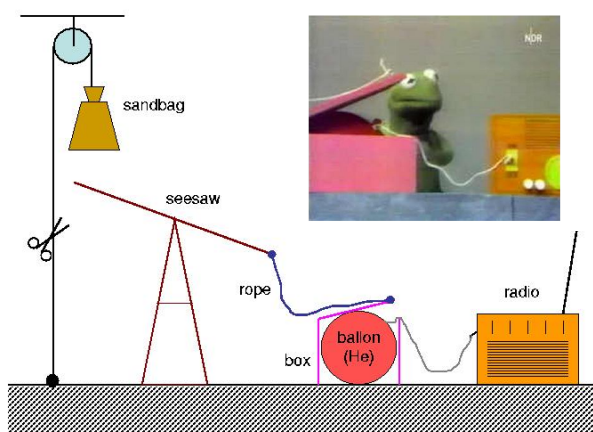


Fig.1 Scheme of the What-Happens-Next-Maschine. Inset: Kermit the Frog in the scene.

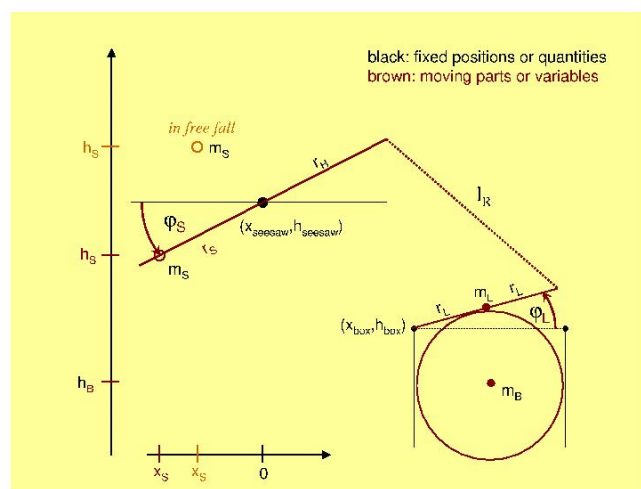


Fig.2 Geometry of the seesaw and the box's lid. Definition of positions, distances and angles.

In the children's television series *Sesame Street* Kermit the Frog, a muppet created by Jim Henson, presented his What-Happens-Next-Machine. Although he proclaimed having constructed it to avoid walking from here to there to turn on his radio, the purpose of the scene, of course, lies in conveying to the spectator the concept of a chain reaction. More spectacular chain reactions are now often demonstrated in science museums [1] and TV shows [2]. The What-Happens-Next-Machine, however, is a - if not *the* - historical, famous or notorious example. The setup is meant to function as follows: A string being cut, a sandbag hung from a pulley drops onto a seesaw. To the other end

of the seesaw a rope is tied which lifts the lid of a box containing a balloon, preferably filled with helium. From the balloon a string had already been trailing out of the box and is attached to the switch of a radio. So as the lid opens and the balloon rises, at the point the strings is pulled straight up the radio is turned on. But, fitting the typical irony of Sesame Street, even though Kermit tries to save whatever possible, nearly every step - except for the balloon floating up (with some delay) - is malfunctioning [3]. Thus, albeit for the good entertainment the flawed performance provides, unfortunately the spectator does not get to see the before described and intended chain reaction. Without malfunctions, how fast would it go?

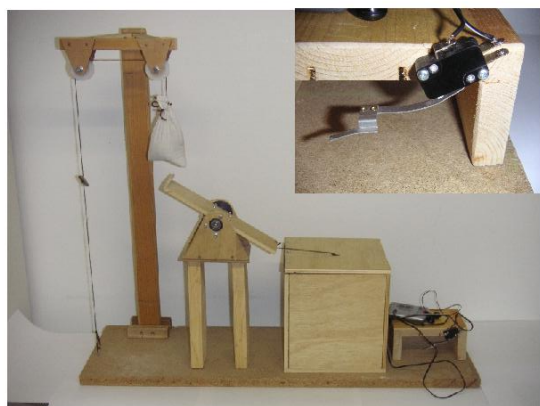


Fig.3 What-Happens-Next-Machine built by students in Konstanz 2009. Slightly different from the original and theoretically discussed version, the rope is attached at the middle of the box's lid and the seesaw's little edge will prevent the sandbag from sliding. The inset shows a rocker switch a straightening balloon string can actually operate.)



Fig.4 Here the sandbag has fallen, turned over the seesaw and opened the lid. In this photo taken during setup there is no balloon yet. The seesaw need not pull the lid up to the vertical. The balloon can be smaller than the box and come out sideways. Anyway, if the lid is pulled strongly enough at the beginning, it has enough momentum to move on up to vertical.

While it can also be a nice task for students to build and run the machine, this article focusses on calculating the motion. Referring to every-day life phenomena or using toys [4] can make physics courses and exercises more appealing. The difficulty often is that one physical concept in its pure form is insufficient to explain the behaviour. A calculation of the What-Happens-Next-Machine as well has to begin by making appropriate idealizations. It can, however, provide a challenging exercise for second-year students of physics. In analytical mechanics textbook examples may fall short of actually conveying the virtue of the Lagrange formalism, because the posed problems of calculating something's motion can just as well be solved by Newtonian concepts, evaluating forces and using energy and momentum conservation. In the setup considered here in the connection of the seesaw to the also rotating lid by the rope an unexpected

complexity is concealed. Finally, numerics will be used making the theoretical problem also a programming exercise.

2. Lagrangian

The setup is drawn in Fig.1 and a close-up with labels is given in Fig.2. We need: fixed quantities:

- g : constant of gravitation, 9.81 m s^{-2}
- m_S : mass of the sandbag (considered a point mass)
- r_H : length of the right half of the seesaw
- l_R : length of the rope (straightened)
- r_L : half edge of the box, and thus also of the lid (assumed square)
- m_L : mass of the box's lid
- I_L : moment of inertia of the box's lid with respect to its hinge; $I_L = m_L \cdot (2r_L)^2/3$
- r_B : radius of the balloon (assumed a sphere); we set $r_B = r_L$
- ρ_{Air} : density of air, 1.29 kg m^{-3} ρ_{He} : density of helium, 0.18 kg m^{-3}

variables:

- x_S : horizontal position of the sandbag counted from the middle of the seesaw
- h_S : vertical position (height) of the sandbag also counted from the middle of the seesaw
- r_S : distance of the sandbag from the middle of the seesaw when the two are in contact
- φ_S : tilt angle of the seesaw, zero=horizontal, pos.=left side is down, neg.=left side is up
- φ_L : opening angle of the lid, counted positive when opened from horizontal
- h_B : height of the balloon (center)

The following energies are involved:

<u>component</u>	<u>potential</u>	<u>kinetic</u>
sandbag	$m_S g h_S$	$\frac{m_S}{2} (\dot{x}_S^2 + \dot{h}_S^2)$
lid	$m_L g r_L \sin \varphi_L$	$\frac{I_L}{2} \dot{\varphi}_L^2$
balloon	$\frac{4}{3}\pi r_B^3 (\rho_{He} - \rho_{Air}) g h_B$	$\frac{1}{2} \frac{4}{3}\pi r_B^3 \rho_{He} \dot{h}_B^2$

$h_S = -r_S \sin \varphi_S$ if the sandbag is on the seesaw. The kinetic energy of the sandbag can be rewritten as $\frac{m_S}{2}(\dot{r}_S^2 + r_S^2 \dot{\varphi}_S^2)$ if the sandbag and the seesaw are moving together. The potential energy of the balloon accounts for buoyancy. The seesaw is regarded as massless (that is negligible mass as compared to the sandbag). The box is fixed to the ground, only the lid moves. The rope is assumed massless and the mass of the balloon's rubber skin is neglected, too [5]. There is no friction in the hinges of the seesaw and the lid and as well no sliding friction is considered should the sandbag slide down the seesaw. The Lagrangian [6] (for the sandbag in contact with the seesaw) is therefore put up as:

$$\mathcal{L} = \frac{m_S}{2}(\dot{r}_S^2 + r_S^2 \dot{\varphi}_S^2) + m_S g r_S \sin \varphi_S + \frac{I_L}{2} \dot{\varphi}_L^2 - m_L g r_L \sin \varphi_L + \frac{1}{2} \frac{4}{3}\pi r_B^3 \rho_{He} \dot{h}_B^2 - \frac{4}{3}\pi r_B^3 (\rho_{He} - \rho_{Air}) g h_B \quad (1)$$

In the following we shall, however, consider \mathcal{L} without the balloon's contributions. To neglect the pressure the balloon due to buoyancy exerts from below onto the lid, seems a realistic assumption. The balloon will therefore only follow the motion of the lid if it can

rise fast enough. We further assume that the balloon does not bounce off downwards when it hits the lid, but that its motion is completely damped out in this case. Letting aside the balloon, following the Lagrange formalism we deduce:

$$\begin{aligned} & \left(\frac{\partial \mathcal{L}}{\partial r_S} - \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{r}_S} \right) \delta r_S + \left(\frac{\partial \mathcal{L}}{\partial \varphi_S} - \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\varphi}_S} \right) \delta \varphi_S + \left(\frac{\partial \mathcal{L}}{\partial \varphi_L} - \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\varphi}_L} \right) \delta \varphi_L = \\ & (m_S r_S \dot{\varphi}_S^2 + m_S g \sin \varphi_S - m_S \ddot{r}_S) \delta r_S + (m_S g r_S \cos \varphi_S - 2m_S r_S \dot{r}_S \dot{\varphi}_S - \\ & m_S r_S^2 \ddot{\varphi}_S) \delta \varphi_S - (m_L g r_L \cos \varphi_L + I_L \ddot{\varphi}_L) \delta \varphi_L = 0 \end{aligned} \quad (2)$$

t is time. r_S is an independent variable, whence we get

$$\ddot{r}_S = g \sin \varphi_S + r_S \dot{\varphi}_S^2 \quad (3)$$

as a first differential equation or equation of motion. With the rope straight, φ_S and φ_L are not independent. We choose to take φ_L as a function of φ_S . The geometric relation is given in an attachment. Then $\delta \varphi_L = \frac{d\varphi_L}{d\varphi_S} \delta \varphi_S$, $\dot{\varphi}_L = \frac{d\varphi_L}{d\varphi_S} \dot{\varphi}_S$ and $\ddot{\varphi}_L = \frac{d^2\varphi_L}{d\varphi_S^2} \dot{\varphi}_S^2 + \frac{d\varphi_L}{d\varphi_S} \ddot{\varphi}_S$. The derivatives $\frac{d\varphi_L}{d\varphi_S}$ and $\frac{d^2\varphi_L}{d\varphi_S^2}$ are evaluated numerically in an actual calculation. Thus a second equation of motion follows from (2):

$$\ddot{\varphi}_S = \frac{m_S g r_S \cos \varphi_S - 2m_S r_S \dot{r}_S \dot{\varphi}_S - (m_L g r_L \cos \varphi_L + I_L \frac{d^2\varphi_L}{d\varphi_S^2} \dot{\varphi}_S^2) \frac{d\varphi_L}{d\varphi_S}}{m_S r_S^2 + I_L \left(\frac{d\varphi_L}{d\varphi_S} \right)^2} \quad (4)$$

The functionality $\varphi_L(\varphi_S)$ is a constraint in the sense of the Lagrange formalism. It takes the form of an equality if the rope is straight. A non-holonomous constraint, nevertheless, is also always present if the rope is loose, namely that the right endpoint of the seesaw and the right edge of the lid cannot be more than a distance of l_R apart. Even if here we do not handle the balloon as part of one complete Lagrangian, there is an also non-holonomous constraint on its motion. It cannot exceed a certain height determined by the lid, whereas it may well stay below that limit. Geometric considerations concerning this point are given in an attachment. Furthermore, not including the balloon pressing against the lid from underneath into the equations of motion, care must be taken not to let the lid drop below its initial position on top of the balloon. The integration of (3) and (4) is performed numerically, in the most simple manner in the attached program. More advanced methods like, for example, the Runge-Kutta scheme, could of course be employed.

3. Impact

Calculating the free fall of the sandbag as well as the time and position of its hitting the seesaw is trivial. At the beginning the seesaw can be at rest at any angle the length of the rope allows. As long as or if the rope is not straight our massless seesaw will just give way to the free falling sandbag. However, the instant the rope straightens or is already straight when the sandbag hits the seesaw, because of suddenly the weight of the lid pulling there will be a discontinuity in the velocities, which must be determined apart from equations of motion like (3) and (4). This turned out to be the most difficult, and

to my opinion still somewhat ambiguous aspect of the problem. For reasons explained later the more general case is investigated that the lid can already be moving when the rope straightens or the sandbag hits the seesaw. Furthermore can the sandbag also have a horizontal velocity in its free fall. As there is nothing to stop it, the velocity of the sandbag along the seesaw v_{\parallel} is conserved and assigned to \dot{r}_S at impact.

$$\dot{r}_S = -\dot{x}_S \cos \varphi_S - \dot{h}_S \sin \varphi_S \quad (5)$$

But what about the initial angular velocity of the seesaw immediately after impact? We shall assume an inelastic collision insofar as the sandbag never bounces off upwards from the seesaw. Immediately after impact the seesaw and the sandbag move together (later it is checked whether the vertical velocity from the turning and centrifugal motion would exceed free fall and eventually the sandbag is allowed to loose touch with the seesaw). Both kinetic energy and angular momentum cannot be conserved in the collision. Drawing the analogy to the one-dimensional inelastic collision where the two bodies stick together afterwards, momentum is conserved, but part of the kinetic energy goes into deformation and heat, the logical decision in our case is to require conservation of angular momentum. However, as the sandbag on the seesaw and the lid do not turn around the same center, the definition of angular momentum is not necessarily clear here. It further only imports at the singular moment of impact. (The motion afterwards of all parts together as calculated from the Lagrangian obeys energy conservation.)

Our treatment of the impact is therefore based on the following very elementary considerations ‡: The instant the sandbag hits and/or the rope straightens, the pulling lid acts like a hypothetical mass on the seesaw at distance r_H from the center. The angular momentum the lid has with respect to its hinge can instead be taken as that of one third of the mass sitting at its end. Therefore decompose $I_L \dot{\varphi}_{L,before}$ into a lever arm $2r_L$ and momentum perpendicular to it $p_{\perp,L} = \frac{I_L \dot{\varphi}_{L,before}}{2r_L}$. However, now in order to find the part having an effect at the other end of the rope tied to the seesaw, the momentum has to be viewed as made up of two in general non-perpendicular components along the lid and along the rope, the latter being $p_{R,L} = \frac{I_L \dot{\varphi}_{L,before}}{2r_L \sin \alpha}$. How to evaluate the angle α is also given in an attachment. At the seesaw this momentum translated along the rope with lever arm r_H makes up an angular momentum $\frac{I_L \dot{\varphi}_{L,before} r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha}$ (Fig.5). After

‡ Nevertheless, conserving the velocity of the sandbag along the seesaw and for the rotations angular momentum in the form $m_S r_S^2 \dot{\varphi}_S + I_L \dot{\varphi}_L$ does *not* produce spurious results (r_S and $\dot{\varphi}_S$ before the collision just describe the sandbag at the end of its free fall in polar coordinates, $\dot{\varphi}_L$ before is known, afterwards $\dot{\varphi}_L = \dot{\varphi}_L(\varphi_S, \dot{\varphi}_S)$, thus only $\dot{\varphi}_S$ needs to be determined). Neither does conserving kinetic energy of rotational motion $\frac{m_S}{2} r_S^2 \dot{\varphi}_S^2 + \frac{I_L}{2} \dot{\varphi}_L^2$ produce any qualitatively or obviously impossible behaviour (with in general the rope at oblique angles to the seesaw and the lid, forces perpendicular to one can well be along the other, and thus conservation of the sum of angular momenta of each around their hinge need not necessarily be expected, which would leave energy as a quantity eventually to be conserved). Attempting to evaluate velocities after the collision by normal momentum conservation together with the constraint that afterwards the sandbag on the seesaw and the lid at least momentarily move together does lead to contradictions, even if the angles $\varphi_S(t)$ and $\varphi_L(t)$ do not show them. There is more kinetic energy after the collision than before. And this does produce cases where the sandbag bounces off the seesaw with an upward velocity component.

the collision the change of φ_L is determined by that of φ_S , nevertheless, the "transfer coefficient" for angular momentum through the rope remains the factor $\frac{r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha}$. With $v_\perp = \dot{x}_S \sin \varphi_S - \dot{h}_S \cos \varphi_S$ the velocity of the sandbag perpendicular to the seesaw before, to solve for $\dot{\varphi}_S$ immediately after impact we have the following equation:

$$m_S r_S v_\perp + \frac{I_L \dot{\varphi}_{L,before} r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha} = \left(m_S r_S^2 + \frac{I_L r_H \sin(\alpha + \varphi_S - \varphi_L) \frac{d\varphi_L}{d\varphi_S}}{2r_L \sin \alpha} \right) \dot{\varphi}_S \quad (6)$$

The first time the sandbag hits when it comes from vertical free fall and the lid is still at rest, we have $\dot{x}_S = 0$ and $\dot{\varphi}_{L,before} = 0$ at impact. Of course, the argument could have been led the other way round, first replacing m_S at r_S by some mass turning at r_H on the seesaw, translating a momentum component down the rope to the lid and establishing conservation of angular momentum around the hinge of the lid. The results for $\dot{\varphi}_S$ and $\dot{\varphi}_L$ after the collision would have been the same.

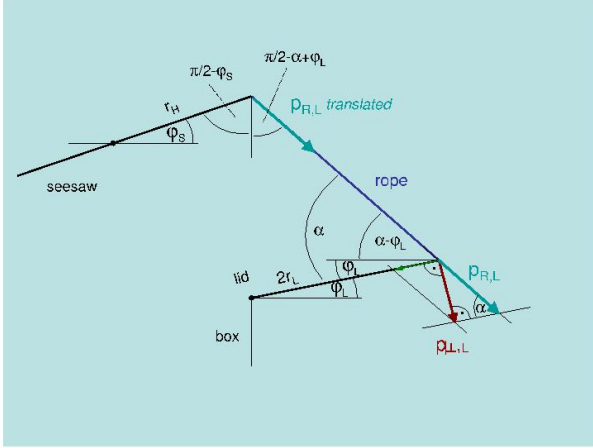


Fig.5 Determining angles and evaluating the momentum component of the lid along the rope.

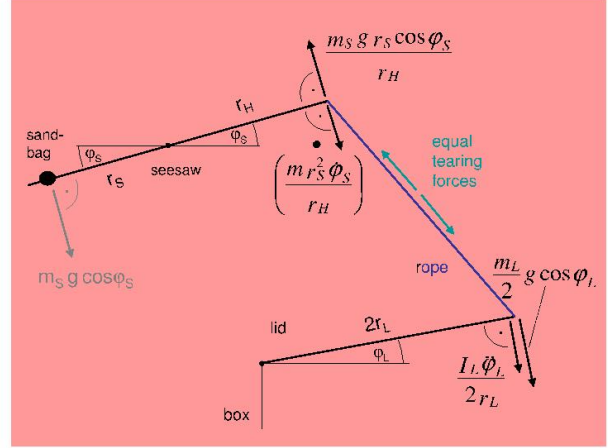


Fig.6 Gravitational and acceleration forces and tearing forces on the rope.

4. Torques, forces and energy

In this section it shall be sought whether the equation of motion could have been deduced by more elementary means than the Lagrange formalism. With the sandbag on the seesaw the sum of kinetic and potential energies is

$$E = \frac{m_S}{2} (\dot{r}_S^2 + r_S^2 \dot{\varphi}_S^2) - m_S g r_S \sin \varphi_S + \frac{I_L}{2} \dot{\varphi}_L^2 + m_L g r_L \sin \varphi_L \quad (7)$$

Requiring energy conservation leads to:

$$0 = \frac{dE}{dt} = m_S \dot{r}_S \ddot{r}_S - m_S r_S \dot{r}_S \dot{\varphi}_S^2 - m_S g \dot{r}_S \sin \varphi_S + 2 m_S r_S \dot{r}_S \dot{\varphi}_S^2 + m_S r_S^2 \dot{\varphi}_S \ddot{\varphi}_S - m_S g r_S \dot{\varphi}_S \cos \varphi_S + I_L \dot{\varphi}_L \ddot{\varphi}_L + m_L g r_L \dot{\varphi}_L \cos \varphi_L \quad (8)$$

where the term $m_S r_S \dot{r}_S \dot{\varphi}_S^2$ has been split into a negative and twice the positive contribution. Now using the knowledge that the radial motion of the sandbag will

follow the respective component of the gravitational force and the centrifugal force, further demand that the first three terms in (8) and the rest be zero each on its own. Dividing by $m_S \dot{r}_S$ or $\dot{\varphi}_S$, respectively, and expressing $\dot{\varphi}_L$ and $\ddot{\varphi}_L$ by derivatives and $\dot{\varphi}_S$ and $\ddot{\varphi}_S$ as before for the motion with the rope straight, this will reproduce (3) and (4).

However, as likely if not more likely than by putting up energy conservation, one would approach a mechanics problem with levers and ropes by looking at forces and torques. The following considerations are still restricted to the motion when the sandbag is in touch with the seesaw and the rope is straight. As explained earlier, the first equation of motion (3) for \ddot{r}_S is rather obviously written down. The torques determining the angular accelerations $\ddot{\varphi}_S$ and $\ddot{\varphi}_L$ are more difficult to find. The time derivative of the sandbag's angular momentum $m_S r_S^2 \dot{\varphi}_S$ is $m_S r_S^2 \ddot{\varphi}_S + 2m_S r_S \dot{r}_S \dot{\varphi}_S$. Like in the last section the change in angular momentum of the lid is taken into account as seen at the other end of the rope. Therefore with respect to the seesaw's center this is $I_L \ddot{\varphi}_L \frac{r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha}$. The component of the gravitational force on the sandbag which leads to angular acceleration is $m_S g r_S \cos \varphi_S$. For the torque m_L 's gravitation exerts on the lid replace the lid by half the mass $\frac{m_L}{2}$ at the end of an otherwise massless lid. As force component perpendicular to the lid there you have $\frac{m_L}{2} g \cos \varphi_L$; multiply by $2r_L$ to get the torque. This torque translates into an effective one $\frac{m_L}{2} g \cos \varphi_L \cdot 2r_L \cdot \frac{r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha}$ at the other end of the rope up at the seesaw, which is, of course, opposed to the sandbag's. The seesaw and the lid are literally tied together and therefore the available torques together have to provide the changes in angular momentum taken together:

$$m_S r_S^2 \ddot{\varphi}_S + 2m_S r_S \dot{r}_S \dot{\varphi}_S + I_L \ddot{\varphi}_L \cdot \frac{r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha} = m_S g r_S \cos \varphi_S - \frac{m_L}{2} g \cos \varphi_L \cdot 2r_L \cdot \frac{r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha} \quad (9)$$

We checked numerically that $\frac{d\varphi_L}{d\varphi_S} = \frac{r_H \sin(\alpha + \varphi_S - \varphi_L)}{2r_L \sin \alpha}$. And when again $\ddot{\varphi}_L = \frac{d^2\varphi_L}{d\varphi_S^2} \dot{\varphi}_S^2 + \frac{d\varphi_L}{d\varphi_S} \ddot{\varphi}_S$ is implied, (9) becomes identical to (4). Setting up the equation of motion for $\ddot{\varphi}_S$ from forces and torques one is likely to forget the term $2m_S r_S \dot{r}_S \dot{\varphi}_S$, which looks like a Coriolis force [7], because (3) already seems to cover effects associated to the radial motion. Instead of projecting the lid's change in angular momentum into an acceleration of rotational motion of the seesaw, one could decompose forces that lead to the respective torques at the right end of the seesaw and at the end of the lid into parts along the seesaw or lid and along the rope and say that the tearing force on the rope is equal in both directions (Fig.6). The acceleration forces are against the sense of the angles, but an equivalent force on the right side of the seesaw to the weight of the sandbag on the left has to point upwards. Further r_S/r_H is for changing the lever arm of the sandbag from r_S to r_H and $\sin(\alpha + \varphi_S - \varphi_L)$ and $\sin \alpha$ are the already known geometrical factors from the parallelograms of forces (or momenta) to get parts along the rope.

$$\frac{1}{\sin \alpha} \left(\frac{m_L}{2} g \cos \varphi_L + \frac{I_L \ddot{\varphi}_L}{2r_L} \right) = \frac{m_S g r_S \cos \varphi_S - m_S r_S^2 \ddot{\varphi}_S - 2m_S r_S \dot{r}_S \dot{\varphi}_S}{r_H \sin(\alpha + \varphi_S - \varphi_L)} \quad (10)$$

(10) is the same as (9).

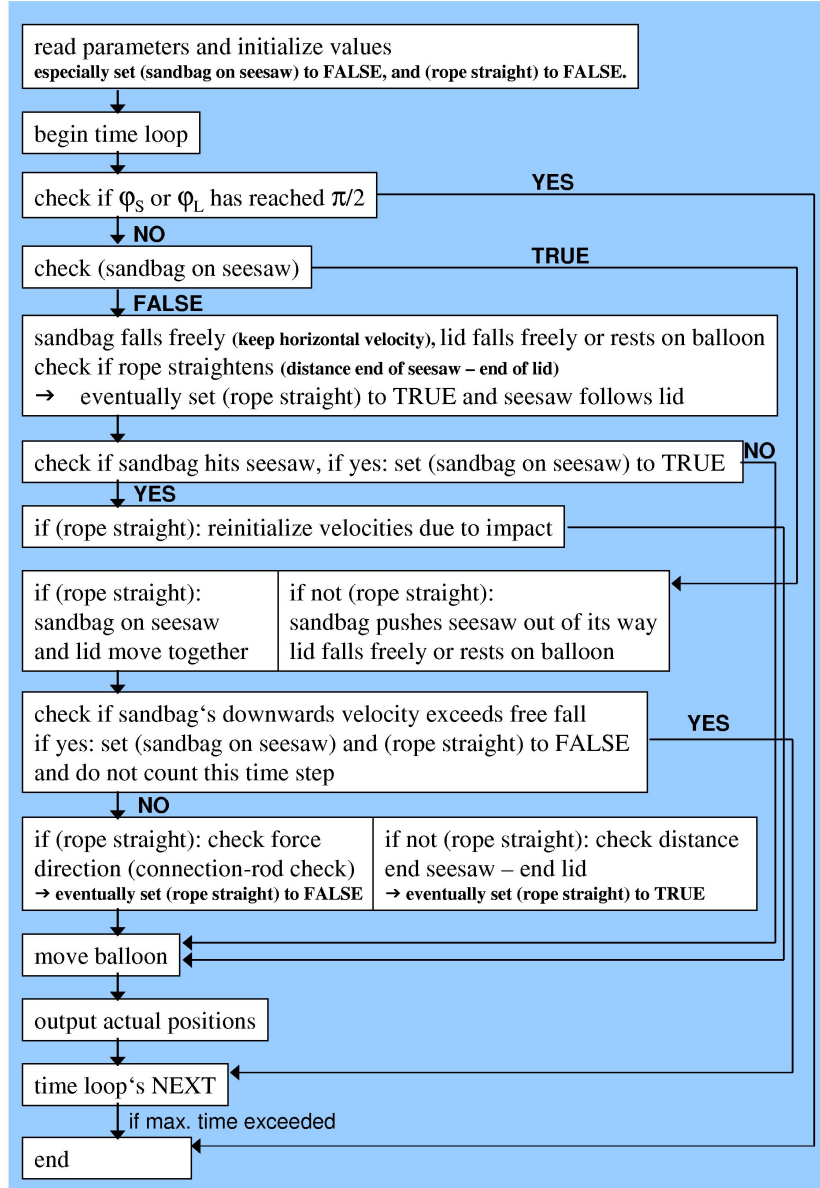


Figure 7. Flow diagram for programming.

5. Cases

One further difficulty, which shall be called the "connecting-rod problem", has so far been overlooked. Of course, this will depend on the parameters, that is weights, lengths and initial angles. With the weight of the lid pulling down, one naturally expects the angular motion to slow down, that is $\ddot{\phi}_S$ and $\ddot{\phi}_L$ become negative. The direction of $\frac{d}{dt}(\frac{m_{sr}^2 \dot{\phi}_S}{r_H})$ in Fig.6 because of the second contribution besides the one with $\ddot{\phi}_S$ in it, $2m_{sr} \dot{r}_S \dot{\phi}_S$, will not necessarily be reversed. Furthermore, with directions

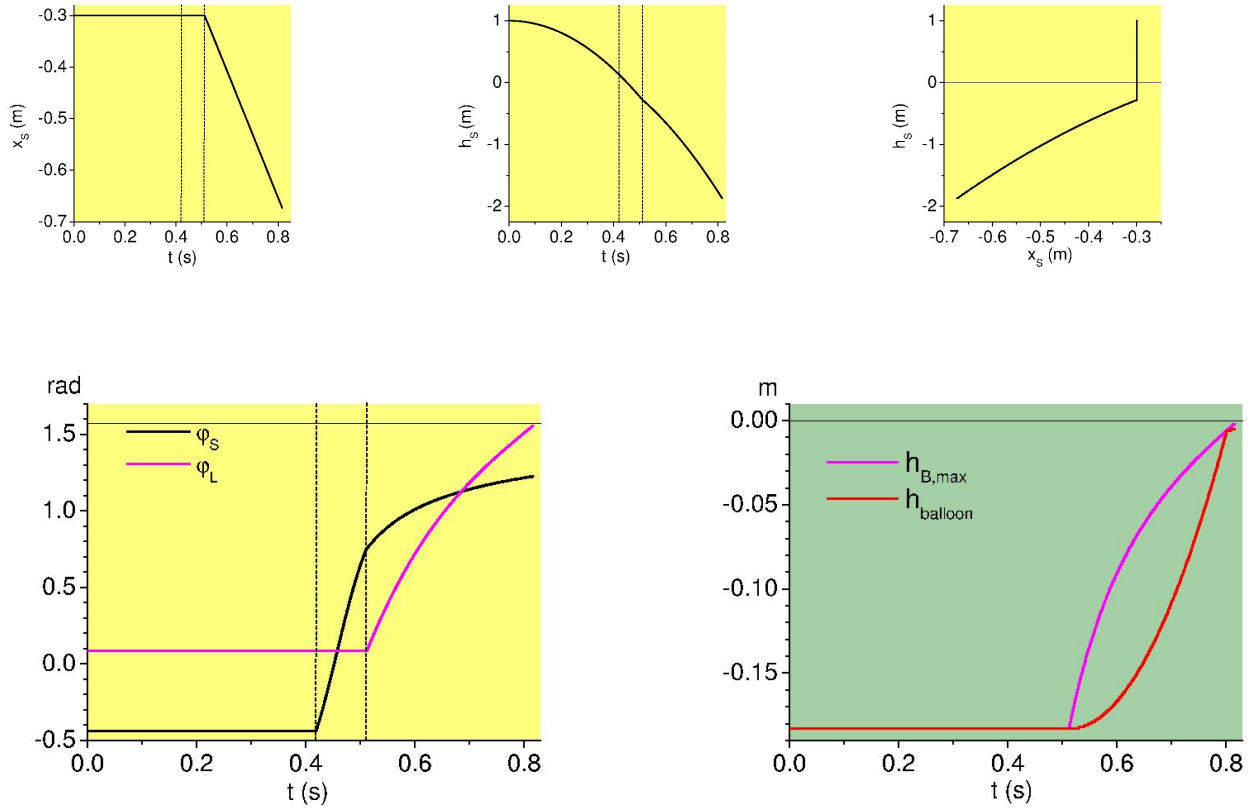
of forces at the end of the seesaw as in Fig.6 there is no reason why we should not have $\frac{d}{dt}(\frac{m_S r_S^2 \dot{\varphi}_S}{r_H}) > \frac{m_S g r_S \cos \varphi_S}{r_H}$. Then Fig.6 and (10) imply that $\ddot{\varphi}_L < 0$ and $\frac{I_L |\ddot{\varphi}_L|}{2r_L} > \frac{m_L}{2} g \cos \varphi_L$. (We shall not allow somersaults, that is we only regard $\varphi_S < \pi/2$ and $\varphi_L < \pi/2$. At $\varphi_S = \pi/2$ the sandbag would drop from the seesaw anyway. And the lid of the box is assumed to engage when it reaches the vertical position. The projection factors $\sin \alpha$ and $\sin(\alpha + \varphi_S - \varphi_L)$ are always positive; the rope cannot come below the lid or above the right side of the seesaw.) A constellation with $\frac{I_L |\ddot{\varphi}_L|}{2r_L} > \frac{m_L}{2} g \cos \varphi_L$ would mean that, instead of tearing, forces would be pushing into the rope from both ends. If then we solved (3) and (4) assuming the distance between the right end of the seesaw and the end of the lid constant, namely the length l_R , we would take the rope for a connecting rod and say that the lid having aquired enough angular momentum could then push against the seesaw from below via the "rope". In this case, in fact, the rope will loosen. The motion of the lid and the sandbag has to be separated, each merely further accelerated by the corresponding gravitational force (our massless seesaw giving way to the sandbag), until again the rope possibly straightens. This is why the general case of a horizontal velocity of the sandbag and the lid already moving had been treated at impact. The flow-diagram for integrating the equations of motion step by step in time in a numerical simulation is given in Fig.7.

6. Examples

Four examples of calculations shall now be given. For each, parameters and starting values as defined in section 2 are given. dt is the time step for the calculation. The balloon is in contact with the lid of the box at the beginning.

first example: Parameters: $m_S = 0.6$ kg, $r_H = 0.6$ m, $l_R = 1.0$ m, $r_L = 0.2$ m, $m_L = 0.5$ kg, $x_{box} - x_{seesaw} = 0.73$ m, $h_{seesaw} - h_{box} = 0.33$ m, $dt = 0.001$ s.
Starting values: $x_S = -0.3$ m, $h_S = 1.0$ m, $\varphi_S = -25^\circ$, $\varphi_L = 5^\circ$.

Besides the horizontal and the vertical position of the sandbag in time, we have also plotted its trajectory in space. Seesaw and lid angles over time are united in one plot. The balloon's height as a function of time is drawn together with the height limit imposed by the lid. $t=0$, of course, is the time the sandbag starts falling. At $t=0.42$ s it hits the seesaw. However, the rope is not straight yet, thus the seesaw just gives way to the falling sandbag. It already turns, such that at $t=0.51$ s when the rope straightens and the lid begins to be pulled up, the seesaw "starting" angle has changed from the initially given value. However, here, immediately after the lid is pulled up for the first time, the *connection-rod check* returns *true*, the rope loosens never to become straight again in this example. The most complicated differential equation (4) is only needed for a single time-step in this calculation! The one impact has given the lid enough angular momentum. It reaches the vertical position ($\varphi_L = \pi/2$) at $t=0.82$ s.

**Fig.8.** First example.

Note that by this time the sandbag is on the seesaw's left arm 2 meters ($\sqrt{x_S^2 + h_S^2}$) from the center. Our program does not contain a check for the sandbag to reach the end of the seesaw (which could be added without problems, nevertheless). In this example at later times the lid moves independently, and the sandbag dropping from the seesaw would not change that. The lid opens faster than the balloon can rise. Only shortly before the box has fully opened does the balloon touch the lid once again. With the lid in vertical position, the balloon can then rise freely. The time it takes to turn on the radio depends on the length of the balloon string and has not been calculated any more. Remark that the interesting part of the motion from the rope's first straightening until the lid's reaching vertical position only lasts from $t=0.51$ s to $t=0.82$ s, that is 0.31 seconds.

second example: As a second example a case has been sought where the rope stays straight at least for some time while pulling up the lid. Parameters and starting values are the same as in the first example except $l_R = 0.62$ m, $h_S = 0.5$ m and $\varphi_S = -35^\circ$. The sandbag meets the seesaw at $t=0.24$ s, the lid starts moving at $t=0.33$ s and reaches the vertical position at $t=0.54$ s, that is already 0.21s later. The balloon cannot catch up with the lid during that time. At the end the sandbag is 0.6m from the center on the left arm of the seesaw, which is equal to the length of the right arm in this case. From $t=0.49$ s on the sandbag cannot follow the seesaw any more and loses touch for more

than one time intervall (the rope loosens). We only show the two angles φ_S and φ_L as functions of time, however, also compare them to the results that would have been obtained had the impact been calculated following conservation of the sum of angular momenta, energy or linear momenta (see section 3). These would be that the lid reaches the vertical position at $t=0.50\text{s}$, $t=0.47\text{s}$ or $t=0.34\text{s}$, respectively. The last one definitely has to be disregarded as unphysical, though (see section 3).

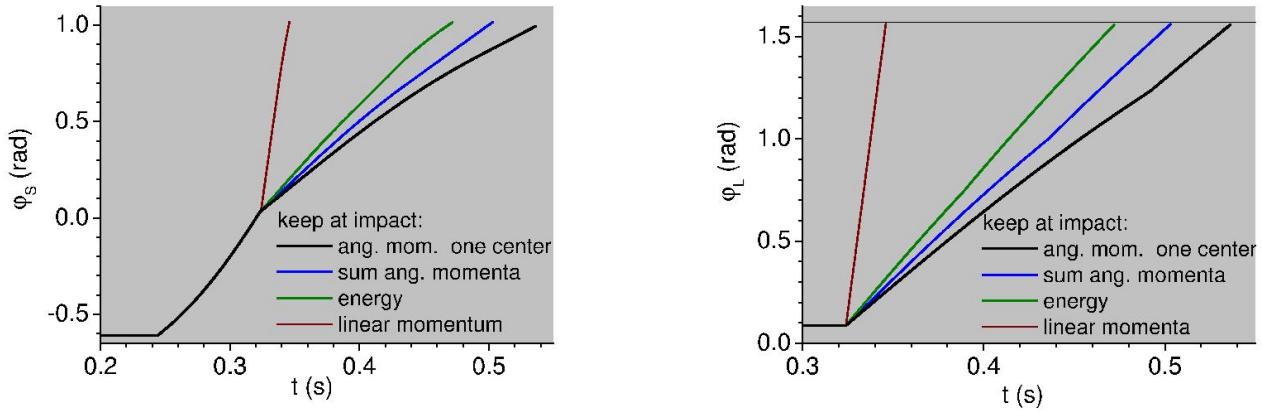


Fig.9. Second example.

third example: Parameters and starting values are the same as in the first example, except $dt = 0.00025\text{ s}$ and at the beginning $h_S = 0.0\text{ m}$, $\varphi_S = 0^\circ$, that is the seesaw is horizontal and the sandbag is just placed on it, not let drop from a height.

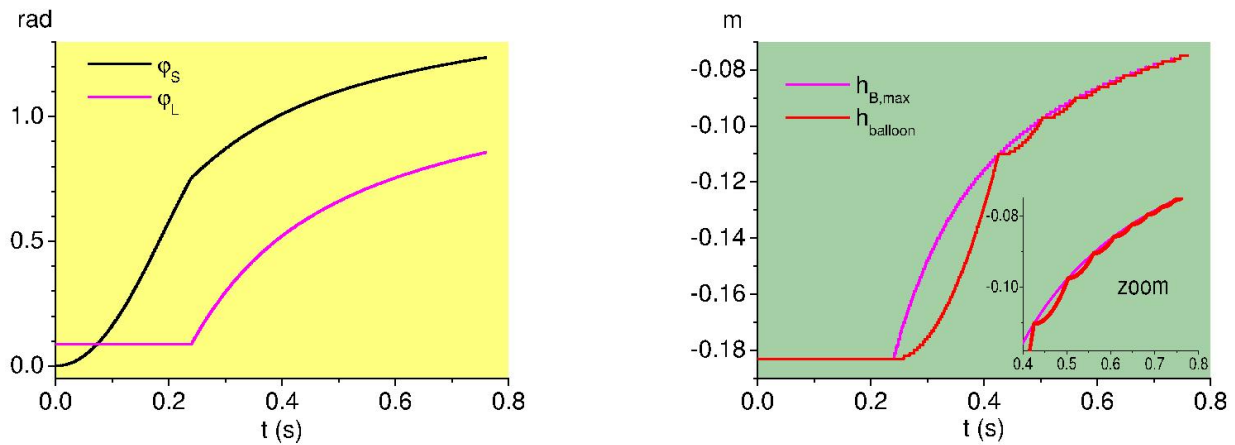


Fig.10. Third example.

This example has been chosen, because the lid opens so slowly that the balloon catches up with it several times until practically staying trapped touching the lid.

Unfortunately, the chain reaction will not come to freeing the ballon and switching on the radio in this case. The seesaw will reach its vertical position at $t=20$ s. However, there we assumed that the sandbag can slide an endless way on it, r_S will be 1949m! The lid will be at $\varphi_L=74^\circ$. At $\varphi_S=\pi/2$ the sandbag finally dropping from the seesaw and the rope loosening, even if one persued this situation which has grown out of proportions, one constitutes that the lid does not have sufficient angular velocity to continue up to vertical position, but will quickly drop back down.

forth example: Parameters: $m_S = 0.7$ kg, $r_H = 0.45$ m, $l_R = 0.9$ m, $r_L = 0.2$ m, $m_L = 0.4$ kg, $x_{box} - x_{seesaw} = 0.64$ m, $h_{seesaw} - h_{box} = 0.29$ m, $dt = 0.001$ s.
Starting values: $x_S = -0.3$ m, $h_S = 0.5$ m, $\varphi_S = -20^\circ$, $\varphi_L = 5^\circ$.

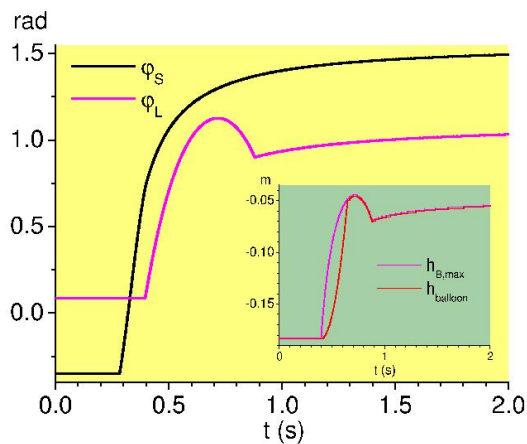


Fig.11. Forth example.

The balloon catches up with the lid at $t=0.64$ s, to be pressed down by it again and then follow it up again staying "glued" underneath it.

7. Conclusions

In conclusion Kermit's What-Happens-Next-Machine has been treated as an analytical mechanics and programming exercise. The two lever arms of the seesaw and the box's lid tied together by the rope can serve as a quite challenging example for finding the equation of motion using the Lagrange formalism. The most difficult point, however, is the decision which quantities are conserved and which are not at impact when the first force on the rope appears. A simulation has been set up and examples with different behaviour have been shown. It has been found that in cases where the counterweight of the falling sandbag is able to fully open the box to free the balloon, the interesting phase of the procedure only lasts some tenths of a second (this cannot be known from the original scene from Sesame Street, because there the machine does not work properly). Some simplifications have been made to be able to solve the problem theoretically (for

Whereas in the third example the rope stayed straight after the first impact at $t=0.33$ s, here at $t=0.40$ s the lid gets such a hard hit that immediately afterwards the rope loosens again (connection-rod condition). The lid jumps up, falls back and only when its fall has again straightened the rope ($t=0.88$ s) is pulled up by the counterweight of the sandbag. However, as in the last example, the seesaw will reach vertical position at about $t=10$ s (r_S will be 344m!), whereas the lid never will.

example: no friction, neglect of the seesaw's mass). At the stage of development, including a mass for the seesaw would mean merely a small extension for who wants to refine the simulation. Attention has to be paid to the case that the seesaw then contributes inertia even if the sandbag is not in touch with it. As has been appreciated by some of our students, in the context of teaching theoretical mechanics, the What-Happens-Next-Machine can be given as an amusing tricky problem.

Acknowledgements

Thanks to Elke Scheer and Wolfgang Belzig, who held the second year's physics lecture to which the What-Happens-Next-Machine was put as a supplementary exercise in the form of a competition. The students Christoph Kölbl and Matthias Haas built the machine shown in Fig.s 3 and 4 and Timm Treskatis' quite complete theoretical analysis drew my attention to some points in which my own original calculation had to be improved.

Attachments:

exercise sheet from physics course (in German); skit of the scene is in English, program in FORTRAN, geometric angle and max. balloon height calculation

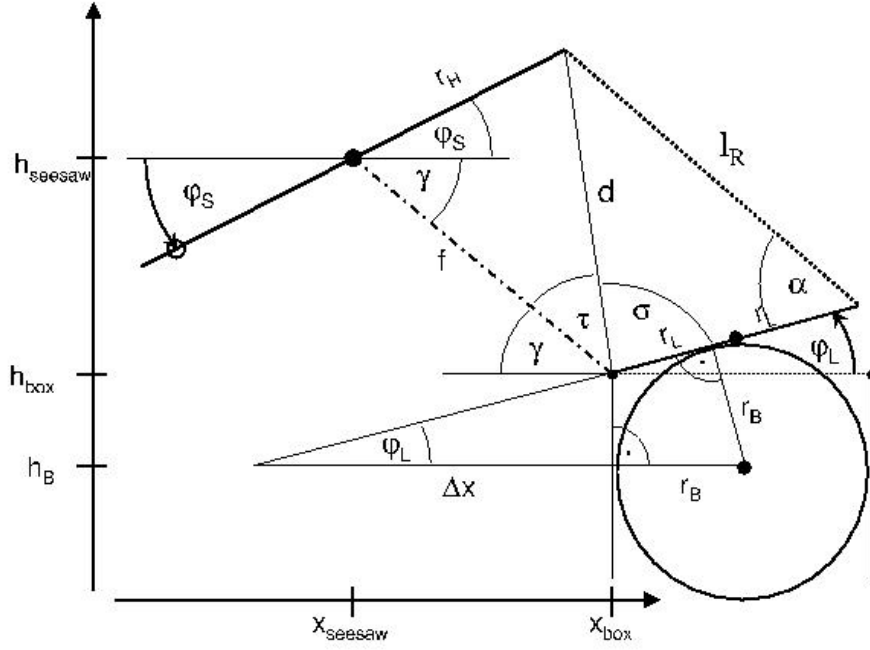
References and Annotations

- [1] for example at NEMO in Amsterdam;
<http://video.aol.com/video-detail/chain-reaction-nemo-amsterdam/517940225>
- [2] *Domino Day* for example.
- [3] just watch the scene yourself; <http://www.youtube.com/watch?v=Yn1rqVdFU0I>
- [4] Güémez J, Fiolhais C and Fiolhais M 2009 *Physics Education* **44** 53
- [5] In practice the volume of helium has to be large enough to lift up the balloon with its skin which in turn requires a large enough box. The one in Fig.s 3 and 4 of about 25cm×25cm proved too small for that reason.
- [6] see any textbook on Theoretical or Analytical Mechanics, for example:
H.Goldstein *Klassische Mechanik*, Aula-Verlag, Wiesbaden 1991.
- [7] see for example: Alonso/Finn *Fundamental University Physics I* chapter 6.4, Addison-Wesley 1980.

Attachments

Mutual dependence of the seesaw's and lid's angles and maximum height of the balloon

Instead of the positions (x_{seesaw}, h_{seesaw}) and (x_{box}, h_{box}) for the center of the seesaw and the hinge of the lid for our programs parameters f and γ are chosen, that is the distance between these two points and the angle the line between them makes with the horizontal. d , σ , τ and α are defined as can be seen from the drawing. Now the cosine- and sine-theorem can be used to get φ_L when given φ_S .



$$d = \sqrt{r_H^2 + f^2 - 2r_H f \cos(\varphi_S + \gamma)}, \quad \tau = \arcsin(r_H \sin(\varphi_S + \gamma) / d),$$

$$\sigma = \arccos((4r_L^2 + d^2 - l_R^2)/(4r_L d)), \quad \varphi_L = \pi - \gamma - \tau - \sigma, \quad \alpha = \arccos((4r_L^2 + l_R^2 - d^2)/(4r_L l_R)).$$

The above calculation holds if the rope is straight. Having expressed d in terms of φ_S , the general constraint on φ_L reads $d^2 + (2r_L)^2 - 2d \cdot (2r_L) \cdot \cos(\pi - \gamma - \tau - \varphi_L) \leq l_R^2$.

As long as the lid has not come to vertical, the balloon must stay below it. We here calculate the maximum possible height of its center. There are slightly different ways to do that, leading to the same result, of course. One could use the fact that the two drawn balloon radii together with the enclosed pieces of the box's wall and lid form a symmetric kite with two right angles. Here use the triangle with angle φ_L formed to the left of the box by the extensions of the lid and the horizontal balloon radius. Putting together $\tan \varphi_L = (h_{box} - h_{B,max})/\Delta x$ and $\sin \varphi_L = r_B/(r_B + \Delta x)$ to eliminate Δx one deduces $r_B + (h_{box} - h_{B,max})/\tan \varphi_L = r_B/\sin \varphi_L$ and so the constraint on the balloon's motion is: $h_B \leq h_{box} - r_B \cdot (1 - \sin \varphi_L)/\cos \varphi_L$.

Program

```

program kermit
implicit none

integer cr,sos,steps,count,straight
double precision hs,xs,phiS,phiL,gamma,f,pi,rL,rB,rH,ms,mL,iL,rs
double precision rhoair,rhohe,tmax,dt,g,vvs,phisp,rspp,alpha
double precision xfs,hfs,xfl,hfl,xsold,t,philp,vhs
double precision hb,vb,hbold,hbl,hbf,dphi,phisold,philold
double precision phisp,d,arccos,hsold,vvsold,vhsold,rsold,rsppold
double precision philplus,philminus,numerator,denominator
double precision philstart,airline,lR,deriv1,deriv2,phisppold
double precision pv,ph,coefa,coefb,coefc,coefd,philppold
common pi,rH,rL,f,gamma,lR

open(11,file='whatnext.inp',status='old')
open(12,file='whatnext.dat',status='unknown')

*****
** This is what the input file 'whatnext.inp' should look like **
*****
**
* 1.0 ; hs = initial height of sandbag in meters *
* -0.3 ; xs = initial horizontal position of sandbag in meters *
* -25.0 ; phiS = initial angle of the seesaw in degrees *
* 5.0 ; phiL = initial angle of the lid in degrees *
* 0.8 ; f = distance center of seesaw - lid's hinge in meters *
* 1.0 ; lR = length of the rope in meters *
* 27.0 ; gamma=angle of line seesaw center-lid hinge to horizontal(deg)*
* 0.2 ; rL = half length of the lid in meters *
* 0.6 ; rH = length of right side of seesaw in meters *
* 0.6 ; ms = mass of the sandbag in kilograms *
* 0.5 ; mL = mass of the lid in kilograms *
* 1.29 ; rhoair = density of air in kilograms per cubic meter *
* 0.18 ; rhohe = density of helium in kilograms per cubic meter *
* 1.0 ; tmax = maximum time for calculation in second *
* 0.001 ; dt = time step in seconds *
**
*****

read(11,*) hsold
read(11,*) xsold
read(11,*) phiS
read(11,*) phiL
read(11,*) f
read(11,*) lR
read(11,*) gamma
read(11,*) rL
read(11,*) rH
read(11,*) ms
read(11,*) mL
read(11,*) rhoair
read(11,*) rhohe
read(11,*) tmax
read(11,*) dt
pi=4.0*atan(1.0)
phiS=phiS/180.0*pi
phiL=phiL/180.0*pi
gamma=gamma/180.0*pi
phisold=phiS
philold=phiL
philstart=phiL
rB=rL
iL=4.0/3.0*mL*rL*rL
g=9.81
vvs=0.0
vvsold=0.0
vhs=0.0
vhsold=0.0

```

```

    phisp=0.0
    philp=0.0
    phispold=0.0
    philpold=0.0
    vb=0.0
    phispp=0.0
    dphi=pi/200.0
    xfs=-f*cos(gamma)+rH*cos(phiS)
    hfs=f*sin(gamma)+rH*sin(phiS)
    xfl=2.0*rL*cos(phiL)
    hfl=2.0*rL*sin(phiL)
    airline=sqrt((xfs-xfl)**2+(hfs-hfl)**2)
    if (airline.gt.lR) then
        print*, 'The rope is too short for these starting parameters.'
        print*, airline
        stop
    endif
    if (phis.lt.0.0) then
        if (hsold.lt.-xsold*tan(phis)) then
            print*, 'sandbag must not start underneath seesaw'
            stop
        endif
    else
        if (hsold.lt.xsold*tan(phis)) then
            print*, 'sandbag must not start underneath seesaw'
            stop
        endif
    endif
    sos=0
    straight=0
    steps=int(tmax/dt)
    t=0.0

    if (abs(phil).le.1.0D-10) then
        hbold=-rB
    else
        hbold=-(1.0-sin(phiL))/cos(phiL)*rB
    endif

    do count=1, steps
        t=t+dt
        cr=0

c stopping condition
        if ((phiL.gt.pi/2.0-dphi).or.(phiS.gt.pi/2.0-dphi)) goto 90

c check if sandbag is on seesaw
        if (sos.eq.1) goto 20

c sandbag and lid move separately
        vvs=vvsold+g*dt
        vhs=vhsold
        hs=hsold-vvsold*dt-0.5*g*dt*dt
        xs=xsold+vhsold*dt
        phiL=phiL+philp*dt
        philp=philp-mL*g*rL/iL*cos(phiL)*dt
        if (phiL.lt.philstart) then
            phiL=philstart
            philp=0.0
        endif
        if (straight.eq.0) then
            phiS=phiS+phis*dt
            xfs=-f*cos(gamma)+rH*cos(phiS)
            hfs=f*sin(gamma)+rH*sin(phiS)
            xfl=2.0*rL*cos(phiL)
            hfl=2.0*rL*sin(phiL)
            airline=sqrt((xfs-xfl)**2+(hfs-hfl)**2)
            if (airline.ge.lR) straight=1
        endif
        if (straight.eq.1) then

```



```

        call machphis(phiL,phiS)
        phisp=(phiS-phisold)/dt
    endif

c check if sandbag has hit seesaw
    if (atan(hs/xs).lt.phiS) goto 30

c initialize velocities at impact
    sos=1
    rs=-xs/cos(phiS)
    rsp=-vhs*cos(phiS)+vvs*sin(phiS)
    if (straight.eq.1) then
c keep angular momentum referred to ONE center
        d=sqrt(rH*rH+f*f-2.0*rH*f*cos(phiS+gamma))
        alpha=arccos((4.0*rL*rL+lR*lR-d*d)/(4.0*rL*lR))
        call machphiL(phiS,phiL)
        call machphiL(phiS+dphi,philplus)
        call machphiL(phiS-dphi,philminus)
        deriv1=(philplus-philminus)/2.0/dphi
        numerator=ms*rs*(vvs*cos(phiS)+vhs*sin(phiS))+(iL*philp*rH*
1      sin(alpha+phiS-phiL))/(2.0*rL*sin(alpha))
        denominator=ms*rS*rS+(iL*rH*sin(alpha+phiS-phiL)*deriv1)/
1      (2.0*rL*sin(alpha))
        phisp=numerator/denominator
        philp=deriv1*phisp
cc if we kept sum of angular momenta
cc sandbag around center of seesaw and lid around its hinge
c      call machphiL(phiS,phiL)
c      call machphiL(phiS+dphi,philplus)
c      call machphiL(phiS-dphi,philminus)
c      deriv1=(philplus-philminus)/2.0/dphi
c      phisp=(ms*rS*(vvs*cos(phiS)+vhs*sin(phiS))+iL*philp)/
c      1      (ms*rS*rS+iL*deriv1)
c      philp=deriv1*phisp
cc if we kept kinetic energy
c      call machphiL(phiS,phiL)
c      call machphiL(phiS+dphi,philplus)
c      call machphiL(phiS-dphi,philminus)
c      deriv1=(philplus-philminus)/2.0/dphi
c      numerator=ms*(vvs*cos(phiS)+vhs*sin(phiS))*2+iL*philp*philp
c      denominator=ms*rS*rS+iL*deriv1*deriv1
c      phisp=sqrt(numerator/denominator)
c      philp=deriv1*phisp
cc if we kept linear momentum - results in nonsense
c      ph=ms*vhs-mL*rL*philp*sin(phiL)
c      pv=-ms*vvs+mL*rL*philp*cos(phiL)
c      call machphiL(phiS,phiL)
c      call machphiL(phiS+dphi,philplus)
c      call machphiL(phiS-dphi,philminus)
c      deriv1=(philplus-philminus)/2.0/dphi
c      coefa=-ms*cos(phiS)
c      coefb=ms*rS*sin(phiS)-mL*rL*sin(phiL)*deriv1
c      coefc=-ms*sin(phiS)
c      coefd=-ms*rS*cos(phiS)+mL*rL*cos(phiL)*deriv1
c      rsp=(ph*coefd-pv*coefb)/(coefa*coefd-coefb*coefc)
c      phisp=(ph*coefc-pv*coefa)/(coefb*coefc-coefa*coefd)
c      philp=deriv1*phisp
    else
        phisp=vvs*cos(phiS)/rs+vhs*sin(phiS)/rs
    endif
c anyway, that's it for this time step
    goto 30

20 continue
c sandbag is on seesaw
    if (straight.eq.1) then
        call machphiL(phiS,phiL)
        call machphiL(phiS+dphi,philplus)
        call machphiL(phiS-dphi,philminus)
        deriv1=(philplus-philminus)/2.0/dphi

```

```

    deriv2=(philplus-2.0*phiL+philminus)/dphi/dphi
    numerator=ms*g*rS*cos(phiS)-2.0*ms*rS*rsp*phisp-
1  mL*g*rL*cos(phiL)*deriv1-iL*phisp*phisp*deriv2*deriv1
    denominator=ms*rS*rS+iL*deriv1*deriv1
    phispp=numerator/denominator
    else
    phispp=(g*cos(phiS)-2.0*rsp*phisp)/rS
    endif
    rspp=rs*phisp*phisp+g*sin(phiS)
    rsp=rsp+rspp*dt
    rS=rS+rsp*dt
    phisp=phisp+phispp*dt
    philp=deriv1*phisp
    phiS=phiS+phisp*dt
    xs=-rS*cos(phiS)
    hs=-rS*sin(phiS)
    vvs=rsp*sin(phiS)+rS*cos(phiS)*phisp
    vhs=-rsp*cos(phiS)+rS*sin(phiS)*phisp
    if (straight.eq.1) then
    call machphil(phiS,phiL)
    else
    philp=philp-mL*g*rL/iL*cos(phiL)*dt
    phiL=phiL+philp*dt
    endif
    if (phiL.lt.philstart) then
    phil=philstart
    philp=0.0
    endif

c check if sandbag falls faster than allowed by free fall
    if (vvs-vvsold.gt.g*dt) then
    sos=0
    straight=0
    t=t-dt
    hs=hsold
    xs=xsold
    vhs=vhsold
    vvs=vvsold
    rs=rsold
    rsp=rsold
    phiS=phisold
    phiL=philold
    phisp=phisold
    philp=philold
    goto 100
    endif

    if (straight.eq.1) then
c connection rod check, check whether rope loosens
    if (ms*rS*rS*phispp+2.0*ms*rs*rsp*phisp.gt.
1  ms*g*rS*cos(phiS)) then
    cr=1
    straight=0
    endif
    else
c distance check, check whether rope straightens
c    print*, 'check distance'
    xfs=-f*cos(gamma)+rH*cos(phiS)
    hfs=f*sin(gamma)+rH*sin(phiS)
    xfl=2.0*rL*cos(phiL)
    hfl=2.0*rL*sin(phiL)
    airline=sqrt((xfs-xfl)**2+(hfs-hfl)**2)
    if (airline.ge.lR) then
    straight=1
    endif
    endif

30 continue
c move the balloon
    hbl=-(1.0-sin(phiL))/cos(phiL)*rB

```

```

        hbf=hbold+vb*dt+0.5*g*(rhoair-rhohe)/rhoair*dt*dt
        if (hbl.lt.hbf) then
            hb=hbl
            vb=0.0
        else
            hb=hbf
            vb=(hb-hbold)/dt
        endif

c update values
        hbold=hb
        xsold=xs
        hsold=hs
        vvsold=vvs
        vhsold=vhs
        rsold=rs
        rspold=rsp
        phisold=phiS
        philold=phiL
        phispold=phisp
        philpold=philp

c output
        write(12,123) t,xs,hs,phiS,phiL,hbl,hb,dble(cr),dble(straight)
123 format (9F8.3)

100 enddo

        print*, 'time out'
        goto 95

90 print*, 'reached vertical position, t',t

95 close(11)
   close(12)
   end

double precision function arccos(x)
implicit none
double precision x,pi,tangens
pi=4.0*atan(1.0)
if (abs(x).le.1.0D-10) then
    arccos=pi/2.0
else
    tangens=sqrt(1.0-x*x)/x
    arccos=atan(tangens)
    if (x.lt.0.0) arccos=arccos+pi
endif
return
end

subroutine machphiS(phiL,phiS)
implicit none
double precision phiS,phiL,pi,lR,rH,rL,f,gamma,dhere,tausigma
double precision arccos,downangle,upangle
common pi,rH,rL,f,gamma,lR
tausigma=pi-phiL-gamma
dhere=sqrt(f*f+4.0*rL*rL-4.0*f*rL*cos(tausigma))
downangle=arccos((dhere*dhere+f*f-4.0*rL*rL)/2.0/dhere/f)
upangle=arccos((dhere*dhere+rH*rH-lR*lR)/2.0/dhere/rH)
phiS=downangle+upangle-gamma
return
end

subroutine machphiL(phiS,phiL)
implicit none
double precision pi,rH,rL,gamma,lR,f,phiL,phiS,arccos,tau,sigma,d
common pi,rH,rL,f,gamma,lR
d=sqrt(rH*rH+f*f-2.0*rH*f*cos(phiS+gamma))
tau=arccos((f*f+d*d-rH*rH)/2.0/f/d)

```

```

sigma=arccos((4.0*rL*rL+d*d-lR*lR)/4.0/rL/d)
phiL=pi-gamma-tau-sigma
return
end

```

7.1. Skit of the scene from Sesame Street

(Kermit is standing next to a rope on a pulley that's attached to a sandbag. The sandbag is suspended over a seesaw. The other end of the seesaw, pointing down, has a string on it attached to the closed lid of a box containing an inflated helium balloon. Its string is trailing out of the box and is tied to the switch of a radio.)

Kermit *(who has a pair of scissors)*: First of all, I'll cut the rope. Then the sandbag will fall on the seesaw. Then that end of the seesaw will go down, and the other end of the seesaw will go up. ...and the balloon will float up in the air! And you will notice that the balloon is tied to the switch of the radio.

Kermit *(going over to the radio)*: You see, in the old days I had to walk all the way over here to turn on my radio. It would tire my flippers. It would waste time. But not anymore ... thanks to the magic of What-Happens-Next! ... First I cut the rope! *(He does ... and the sandbag stays suspended in mid-air.)*

Kermit: And what happens next is ... the sandbag seems to be stuck! The rope must be tangled ... *(He gives it a few good whacks, but it still doesn't fall.)* Oh, well, we'll just skip the sandbag part and go on to the seesaw. I'll just give it a push. *(He does, but it won't budge.)* The seesaw seems to be stuck ... *(He gives a few determined grunts and shoves, but to no avail.)*

Kermit: Oh, well, we'll just ignore the stuck seesaw and move to the box. And what do you know, I'll bet the lid won't open. *(He gets it open on the first try, though.)* Oh, there. *(The balloon refuses to rise.)* I'll give it a few good kicks! *(He does, but the balloon stays put. By now he's really upset.)* Come on, balloon! Are you going to float up in the air or not? *(Kicks it again.)* All right, balloon, I'm giving you one last chance! You float up in that air right now, or I won't be responsible for what happens next! *(He gives the box a vicious kick, and finally the balloon floats up in the air, turning on the radio, which starts playing music.)*

Kermit: Thanks to the magic of What-Happens-Next. Once I get all the bugs out. *(Just then, he sees the balloon carrying the radio away.)*

Kermit: What happens next is I gotta get another radio! *(He jumps as the sandbag suddenly falls on the seesaw, which breaks in two.)*

[adapted from SilveryShoe@aol.com]